

Boundary layer equations

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = 0$$

$$u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} = U_{\infty} \frac{dU_{\infty}}{dx} + \nu \frac{\partial^2 u}{\partial y^2}$$

$$u \frac{\partial T}{\partial x} + v \frac{\partial T}{\partial y} = \alpha \frac{\partial^2 T}{\partial y^2}$$



Similarity Solution

■ similarity variable: a general form $\eta(x, y) = yg(x)$

■ similarity expect: $u(x, y) = U_{\infty}(x)f'(\eta)$

■ transformed stream function:

$$\psi(x, y) = \int u dy + h(x) = \frac{U_{\infty}}{g} f(\eta) + h(x)$$

$$v(x, y) = -\frac{\partial \psi}{\partial x} = -\frac{d}{dx} \left(\frac{U_{\infty}}{g} \right) f - \frac{U_{\infty}}{g} f' yg' - h'$$

$$v(x, 0) = v_0(x) = -\frac{d}{dx} \left(\frac{U_{\infty}}{g} \right) f(0) - h'(x)$$

$$h'(x) = -\frac{d}{dx} \left(\frac{U_{\infty}}{g} \right) f(0) - v_0(x)$$

Similarity Solution

$$v(x, y) = -\frac{d}{dx} \left(\frac{U_\infty}{g} \right) f - \frac{U_\infty}{g} f' y g' + \frac{d}{dx} \left(\frac{U_\infty}{g} \right) f(0) + v_0(x)$$

$$= v_0(x) - \frac{d}{dx} \left(\frac{U_\infty}{g} \right) \{f - f(0)\} - \frac{U_\infty}{g} f' y g'$$

$$u(x, y) = U_\infty(x) f'(\eta)$$

derivatives: $\frac{\partial u}{\partial x} = U_\infty' f' + U_\infty f'' \frac{\partial \eta}{\partial x} = U_\infty' f' + U_\infty f'' \cdot y g'$

$$\frac{\partial u}{\partial y} = U_\infty f'' \frac{\partial \eta}{\partial y} = U_\infty f'' \cdot g$$

X-momentum conservation

$$u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} = U_\infty \frac{dU_\infty}{dx} + v \frac{\partial^2 u}{\partial y^2}$$

$$v(x, y) = v_0(x) - \frac{d}{dx} \left(\frac{U_\infty}{g} \right) \cdot \{f(\eta) - f(0)\} - \frac{U_\infty}{g} \cdot f' \cdot y g'$$

$$u(x, y) = U_\infty(x) f'(\eta)$$

$$\underline{\underline{f''''}} = -\frac{1}{v g} \frac{d}{dx} \left(\frac{U_\infty}{g} \right) \cdot \{f - f(0)\} f'' + \left(\frac{dU_\infty/dx}{v g^2} \right) (f'^2 - 1) + \frac{v_0}{v g} \cdot f''$$

functions of x only functions of η only

Consistence Condition

$$\frac{dU_\infty/dx}{\nu g^2} = \text{constant} = a$$

$$\frac{1}{\nu g} \frac{d}{dx} \left(\frac{U_\infty}{g} \right) = \text{constant} = b \quad \rightarrow$$

$$\frac{v_0(x)}{\nu g(x)} = \text{constant} = B$$

$$U_\infty(x) \propto x^{a/2b-a} \equiv Cx^m$$

$$g(x) \propto x^{a-b/2b-a} = Dx^{(m-1)/2}$$

$$\eta(x, y) = yg(x) = y \sqrt{\frac{U_\infty(x)}{\nu x}}$$

Consistence Condition

$$\frac{dU_\infty/dx}{\nu g^2} = \frac{m}{\nu} \frac{C}{D^2} \equiv m \quad \therefore D = \sqrt{C/\nu}$$

$$\frac{1}{\nu g} \frac{d}{dx} \left(\frac{U_\infty}{g} \right) = \frac{m+1}{2\nu} \frac{C}{D^2} = \frac{m+1}{2}$$

$$g(x) = Dx^{(m-1)/2} = \sqrt{\frac{Cx^{(m-1)}}{\nu}} = \sqrt{\frac{Cx^m}{\nu x}} = \sqrt{\frac{U_\infty(x)}{\nu x}}$$

$$\frac{v_0(x)}{\nu g(x)} = B \Rightarrow v_0(x) = B\nu g(x) \equiv B \sqrt{\frac{\nu U_\infty}{x}}$$

$$B \equiv \frac{v_0(x)}{\sqrt{\nu U_\infty/x}}$$

Blowing/suction condition

$$h'(x) = -\frac{d}{dx} \left(\frac{U_\infty}{g} \right) f(0) - v_0(x) = \left\{ -\frac{m+1}{2} f(0) - B \right\} \sqrt{\nu C x^{m-1}}$$

$$h(x) = \frac{2}{m+1} \left\{ -\frac{m+1}{2} f(0) - B \right\} \sqrt{\nu C x^{m+1}} = \frac{2}{m+1} \left\{ -\frac{m+1}{2} f(0) - B \right\} \sqrt{\nu x U_\infty}$$

$$\psi(x, y) = \frac{U_\infty}{g} f(\eta) + h(x) = \sqrt{\nu x U_\infty} f(\eta) + \frac{2}{m+1} \left\{ -\frac{m+1}{2} f(0) - B \right\} \sqrt{\nu x U_\infty}$$

$$= \sqrt{\nu x U_\infty} \left\{ f(\eta) - \frac{2}{m+1} \left\{ -\frac{m+1}{2} f(0) - B \right\} \right\} = \sqrt{\nu x U_\infty} f(\eta)$$

choose (without loss of generality) $-\frac{m+1}{2} f(0) \equiv B$

Remark

A similarity solution

$$\frac{dU_\infty/dx}{\nu g^2} = m$$

$$\frac{1}{\nu g} \frac{d}{dx} \left(\frac{U_\infty}{g} \right) = \frac{m+1}{2}$$

$$\frac{v_0(x)}{\nu g(x)} = B$$

$$\psi(x, y) = \sqrt{\nu x U_\infty(x)} \cdot f(\eta)$$

$$u(x, y) = U_\infty(x) f'(\eta)$$

$$v(x, y) = -\sqrt{\frac{\nu}{x} U_\infty(x)} \cdot \left\{ \frac{m+1}{2} f(\eta) + \frac{(m-1)}{2} \cdot \eta f'(\eta) \right\}$$

$$\eta(x, y) = yg(x) = y \sqrt{\frac{U_\infty(x)}{\nu x}}$$

exists if $U_\infty(x) \propto x^m$ and $v_0 \propto x^{(m-1)/2}$

Falkner-Skan Equation

$$\underline{\underline{f'''}} = -\frac{1}{\nu g} \frac{d}{dx} \left(\frac{U_\infty}{g} \right) \cdot \underline{\underline{\{f - f(0)\} f''}} + \left(\frac{dU_\infty/dx}{\nu g^2} \right) \underline{\underline{(f'^2 - 1)}} + \frac{\nu_0}{\nu g} \cdot \underline{\underline{f''}}$$

$$2f''' + (m+1)ff'' + 2m(1-f'^2) = 0$$

$$f'(0) = 0$$

$$f'(\infty) = 1$$

$$-\frac{m+1}{2} \cdot f(0) = B \equiv \frac{\nu_0(x)}{\sqrt{\nu U_\infty/x}}$$

$$u(x, 0) = 0$$

$$u(x, \infty) = U_\infty(x)$$

$$v(x, 0) = \nu_0(x)$$

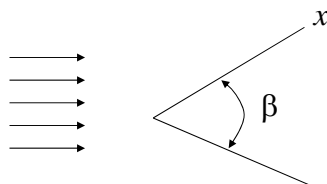
$$u(x, y) = U_\infty(x)f'(\eta)$$

$$-\frac{m+1}{2} f(0) = B = \frac{\nu_0(x)}{\sqrt{\nu U_\infty/x}}$$

Wedge Flows

$$U_\infty(x) \propto x^m$$

$$\frac{dP}{dx} = -\rho U_\infty \frac{dU_\infty}{dx} \neq 0 \quad \text{i.e. } m \neq 0$$



$$m = \frac{\beta}{2\pi - \beta}$$

Thermal Equation

$$u \frac{\partial T}{\partial x} + v \frac{\partial T}{\partial y} = \alpha \frac{\partial^2 T}{\partial y^2}$$

$$\Theta \equiv \frac{T - T_0}{T_\infty - T_0} = \Theta(\eta) \quad , \quad \eta = y \sqrt{\frac{U_\infty(x)}{\nu x}}$$

$$T(y=0) = T_0(x)$$

$$T(y \rightarrow \infty) = T_\infty$$

$$n = \frac{x}{T_\infty - T_0} \frac{d(T_\infty - T_0)}{dx}$$



$$\Theta'' + \frac{m+1}{2} \cdot \text{Pr} \cdot f \Theta' + n \cdot \text{Pr} \cdot (1-\Theta) f' = 0$$

$$\Theta(0) = 0 \quad \Theta(\infty) = 1$$

Friction Coefficient

$$u(x, y) = U_\infty(x) f'(\eta)$$

$$\eta(x, y) = y \sqrt{\frac{U_\infty(x)}{\nu x}}$$

$$\tau_0 = \mu \left(\frac{\partial u}{\partial y} \right)_{y=0} = \mu U_\infty \left(\frac{df'}{d\eta} \right)_{\eta=0} \left(\frac{\partial \eta}{\partial y} \right)_{y=0} = \rho \nu U_\infty f''(0) \sqrt{\frac{U_\infty}{\nu x}}$$

$$C_f = \frac{\tau_0}{\frac{1}{2} \rho U_\infty^2} = 2 f''(0) \sqrt{\frac{\nu}{U_\infty x}} = 2 f''(0) \text{Re}_x^{-1/2}$$

$$C_f \text{Re}_x^{1/2} = 2 f''(0) = \text{constant}$$

$$\text{Re}_x \equiv U_\infty x / \nu$$

Nusselt Number

$$q_0'' = -k \left(\frac{\partial T}{\partial y} \right)_{y=0} = -k(T_\infty - T_0) \left(\frac{d\Theta}{d\eta} \right)_{\eta=0} \left(\frac{\partial \eta}{\partial y} \right)_{y=0} = -k(T_\infty - T_0) \Theta'(0) \sqrt{\frac{U_\infty}{\nu x}}$$

$$\Theta \equiv \frac{T - T_0}{T_\infty - T_0} = \Theta(\eta) \quad h = \frac{q_0''}{(T_0 - T_\infty)} = k \Theta'(0) \sqrt{\frac{U_\infty}{\nu x}} \propto x^{(m-1)/2}$$

$$\eta = y \sqrt{\frac{U_\infty(x)}{\nu x}}$$

$$Nu = \frac{hx}{k} = \Theta'(0) \cdot \sqrt{\frac{U_\infty x}{\nu}} = \Theta'(0) \cdot Re_x^{1/2}$$

$$Nu \cdot Re_x^{-1/2} = \Theta'(0) = \text{constant (function of Pr)}$$

Pressure effect

$$\frac{dP}{dx} = -\rho U_\infty \frac{dU_\infty}{dx} \neq 0 \quad \text{i.e. } m \neq 0$$

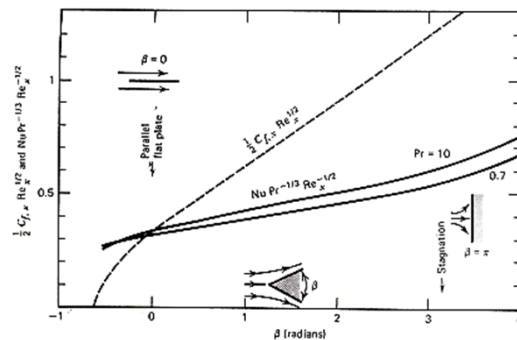


Figure 2.10 Overview of the local friction and heat transfer results for laminar boundary layer flow over an isothermal wedge-shaped body.

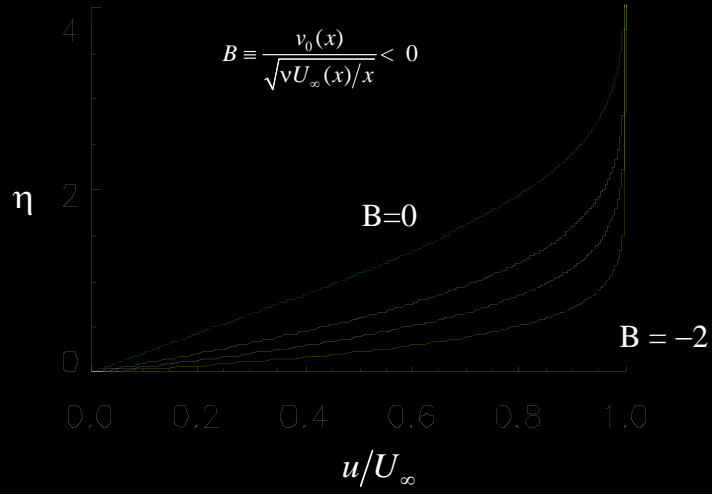
$$U_\infty(x) \propto x^m$$

$$m = \frac{\beta}{2\pi - \beta}$$

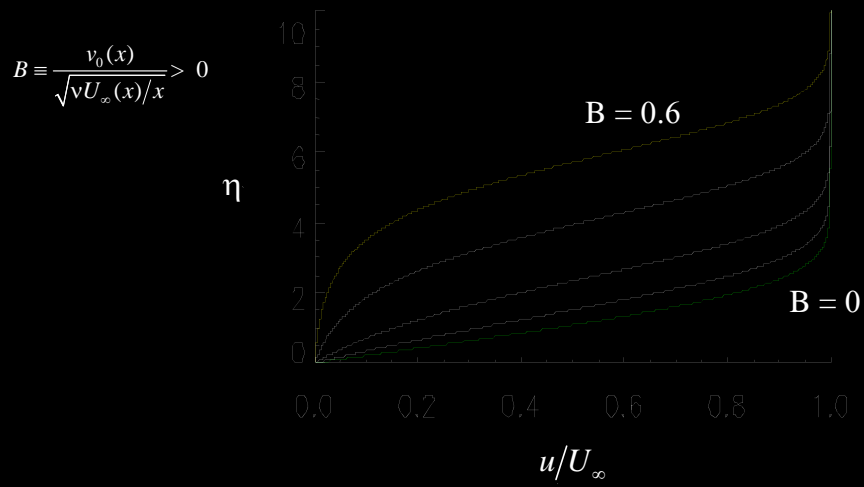
$$\frac{1}{2} C_f Re_x^{1/2} = f''(0)$$

$$Nu Re_x^{-1/2} = \Theta'(0)$$

Suction



Blowing



Blowing/Suction

blowing parameter:

$$B \equiv \frac{v_0(x)}{\sqrt{U_\infty(x)/x}}$$

$$= -\frac{m+1}{2} \cdot f'(0)$$

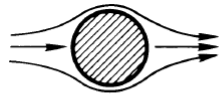
$$\frac{1}{2} C_f \text{Re}_x^{1/2} = f''(0)$$

$$\text{Nu} \text{Re}_x^{-1/2} = \Theta'(0)$$

$\Theta'(0)$

B	$f''(0)$	Pr = 0.7	Pr = 0.8	Pr = 0.9	
-2.5	2.59	1.85	2.097	2.59	Suction
-0.75	0.945	0.722	0.797	0.945	
-0.25	0.523	0.429	0.461	0.523	
0	0.332	0.292	0.307	0.332	impermeable
+0.25	0.165	0.166	0.166	0.165	blowing
+0.375	0.094	0.107	0.103	0.0937	
+0.5	0.036	0.0517	0.0458	0.0356	
+0.619	0	0	0	0	separation

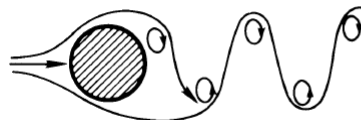
Flow over a circular cylinder/sphere



$\text{Re}_D < 5$ Regime of unseparated flow.



$5 < \text{Re}_D < 40$ A fixed pair of Föppl vortices in the wake

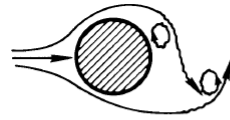


$40 \leq \text{Re}_D < 90$ and $90 \leq \text{Re}_D < 150$

Two regimes in which vortex street is laminar:
Periodicity governed in low Re_D range by wake instability

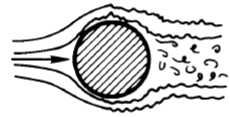
Periodicity governed in high Re_D range by vortex shedding.

Flow over a circular cylinder/sphere



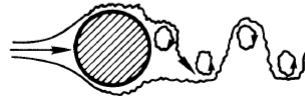
$150 \leq \text{Re}_D < 300$ Transition range to turbulence in vortex.

$300 \leq \text{Re}_D \lesssim 3 \times 10^5$ Vortex street is fully turbulent, and the flow field is increasingly 3-dimensional.



$3 \times 10^5 \gtrsim \text{Re}_D < 3.5 \times 10^6$

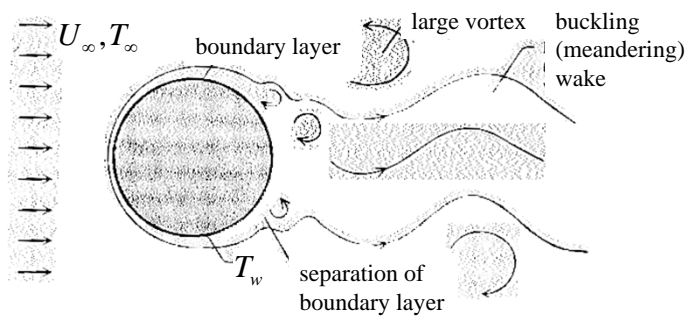
Laminar boundary layer has undergone turbulent transition. The wake is narrower and disorganized. No vortex street is apparent.



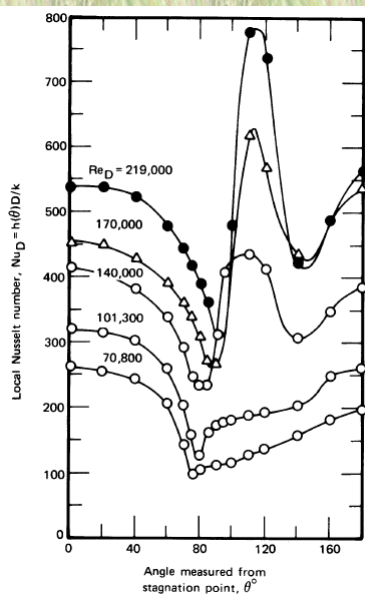
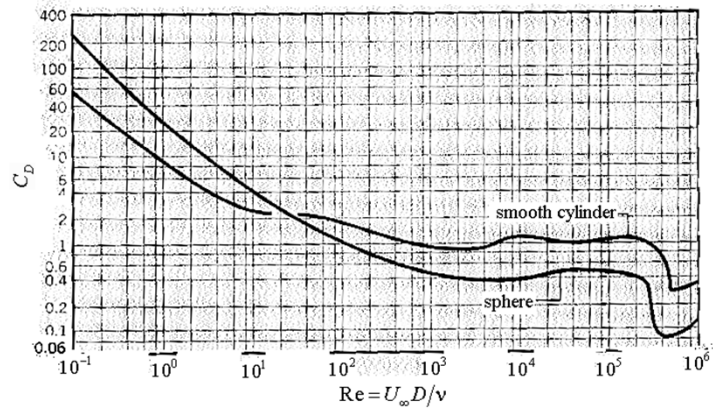
$3.5 \times 10^6 \leq \text{Re}_D < \infty (?)$

Re-establishment of the turbulent vortex street that was evident in $300 \leq \text{Re}_D \lesssim 3 \times 10^5$. This time the boundary layer is turbulent and the wake is thinner.

Single cylinder (or sphere) in cross-flow



Drag coefficient for smooth circular cylinder/sphere



Local Nusselt number for airflow normal to a circular cylinder

- Reynolds-number effect
- boundary layer
- laminar/turbulent
- separation (wake)